

TRF1112 TRF1212 SLWS175A–APRIL 2005–REVISED DECEMBER 2005

Dual VCO/PLL Synthesizer With IF Down-Conversion

FEATURES

- •**Low Phase Noise**
- •**High Dynamic Range Image-Reject**
-
- • **Internal or External AGC Control With Peak Detector and Voltage Reference**
- •
- •
- • **Dual VCO/PLL With On-Chip Resonator For Double Down-Conversion Architecture**

KEY SPECIFICATIONS

- • **S-Band LO Frequency Range: – TRF1112: 1700 to 2400 MHz – TRF1212: 2400 MHz to 3550 MHz**
- • **UHF LO Frequency Range: 325 MHz to 460 MHz**
- •**Phase Noise is 0.5 RMS Typ 100 Hz to 1 MHz**
- •**Rx Noise Figure of 5 dB, Typ**
- • **UHF LO Tuning Step Size of 125 kHz With 18 MHz Reference**
- **Typical Gain of 90 dB, Including 15-dB Loss IF2 SAW Filter**
- •**Input Third Order Intercept Point > 0 dBm**
- •**Input 1-dB Compression Point > –10 dBm**
- •**Gain Control Range of 90 dB Typ**

DESCRIPTION

The TRF1112 / TRF1212 are UHF-VHF down converters with integrated UHF and S-band frequency synthesizers for radio applications in the 2GHz to 4GHz range. The device integrates an image reject mixer, IF gain blocks, automatic gain control (AGC), and two complete phase locked loop (PLL) circuits including: VCOs, resonator circuit, varactors, dividers, and phase detectors.

The TRF1112 / TRF1212 are designed to function as part of Texas Instruments 2.5-GHz and 3.5-GHz complete radio chipsets, respectively. In the chipset, two chips function together to double-down convert **Downconverter EXECUTE:** RF frequencies to an IF frequency that is suitable for **Selectable IF Filters EXECUTE:** The TRETTER MOST baseband modem ADCs. The TRETTER 12 / TRF1212 performs the second down conversion from the first IF frequency (480 MHz typical) to ^a final IF frequency (20-50 MHz). The radio chipset features **Analog Gain Control Range** sufficient linearity, phase noise and dynamic range to **Direct Interface to A/D Direct Interface to A/D** work in single carrier or multi-carrier, line-of-sight or non-line-of-sight, IEEE standard 802.16, BWIF, or proprietary systems. Due to the modular nature of the chipset, it is ideal for use in systems that employ transmit or receive diversity.

TRF1112 / TRF1212 PIN OUT LPCC−48 PACKAGE

BLOCK DIAGRAM

The detailed block diagram and the pin-out of the ASIC are shown in [Figure](#page-1-0) 1 and the Terminal Functions table.

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TERMINAL FUNCTIONS

(1) Current leakage on the order of 10 µA through the capacitor or by any other means from either LF pin can cause false loss of lock signals. The two pull up resistors (R23 and R24) in [Figure](#page-20-0) 20 reduce this sensitivity.

TERMINAL FUNCTIONS (continued)

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ABSOLUTE MAXIMUM RATINGS

(1) Thermal resistance is junction to ambient assuming thermal pad with 16 thermal vias under package metal base see recommended PCB layout (see Figure 20.)

DC ELECTRICAL CHARACTERISTICS

 V_{CC} = 5 V, T = 25°C (unless otherwise noted)

DOWNCONVERTER ELECTRICAL CHARACTERISTICS

 V_{CC} = 5 V, T_A = 25°C, FIF = 480 MHz, IF2 SAW 43.75 MHz unless otherwise stated

DOWNCONVERTER ELECTRICAL CHARACTERISTICS (continued)

 V_{CC} = 5 V, T_A = 25°C, FIF = 480 MHz, IF2 SAW 43.75 MHz unless otherwise stated

SYNTHESIZER #1 (S-BAND PLL) ELECTRICAL CHARACTERISTICS

SYNTHESIZER #2 (UHF-BAND PLL) ELECTRICAL CHARACTERISTICS

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SYNTHESIZER #2 (UHF-BAND PLL) ELECTRICAL CHARACTERISTICS (continued)

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INPUT REFERENCE REQUIREMENTS

(1) Note that for source peak-to-peak voltage of less than 4 V and dc component other than 2.5-V degradation of the close-in phase noise may occur. For oscillators with no dc component, ^a dc voltage may be applied using ^a voltage divider (see the schematic).

AC TIMING, SERIAL BUS INTERFACE

DIGITAL INTERFACE CHARACTERISTICS

AUXILIARY, AGC, AND CONTROL FUNCTIONS

The V_{AGCO} vs V_{AGCI} is the voltage-transfer-function as defined by Table 1 when the AGCO is loaded with 10 kΩ. Note: The RFAGC pin on Texas Instruments RF downconverters (such as: TRF1111, TRF1115, or TRF1216) have an internal load of 10 kΩ and consequently the user should not add ^a separate 10-kΩ load resistor.

Table 1. AGCO Voltage vs AGCI Voltage

FREQUENCY PLAN

The TRF1112 / TRF1212 allow a variety of frequency plans. [Figure](#page-7-0) 2 illustrates the allowable combinations of first and second IFs. However, due to the fact that the chips feature image-reject mixers, significant changes in the frequency plan can result in degradation of image rejection. This phenomenon is captured in [Figure](#page-7-0) 3.

In order to maintain maximum image rejection and LO suppression, a recommended frequency plan is: RxIF1 = 480 MHz, RxIF2 ⁼ 43.75 MHz.

Figure 3. Image Rejection vs IF2

RECEIVE GAIN CONTROL

The TRF1112 / TRF1212 offers two methods for gain control. Gain can be adjusted via an external analog signal (0-3 V) or by using the on-chip detector, voltage reference and operational amplifier.

The gain-response curve is shown in [Figure](#page-8-0) 4 and is designed to be monotonic for a 0-V to 3-V input analog voltage. This voltage control (AGCI) can be used to keep ^a constant peak-to-peak differential voltage output from the TRF1112 / TRF1212 to the baseband processor's ADC over ^a large input signal dynamic range. The recommended TRF1112 / TRF1212 differential output level is 1.2 Vpp. The ASIC AGC output pin (AGCO) can be used to control the gain of ^a front-end downconverter for improved system dynamic range. In order to minimize the receiver's noise figure, the gain is changed in ^a stepped fashion. This means as the input signal level decreases, the gain shifts from the front-end stages to the back-end stages of the chip. This approach allows the noise figure to remain low until large input signals are present.

Closed-Loop AGC

In order to achieve very fast signal acquisition in applications such as burst-mode transmission, Texas Instruments offers ^a receive gain control loop that requires no interaction from the demodulator. The internal loop operates by comparing the output of an internal peak detector to an internal voltage reference and adjusting the gain of the receive chain such that ^a constant voltage is achieved over ^a large input signal dynamic range. The internal AGC speed is set by an external AGC loop filter, the speed of which should be set low enough so that the AGC loop will not remove any carrier AM modulation.

Careful attention to the ASIC architecture enables excellent $3rd$ order intermodulation distortion (IMD) performance over the entire AGC range as shown in [Figure](#page-9-0) 4 and Figure 5. In these figures, VREF refers to the reference voltage setting on the VREF pin which is used to set the output voltage swing when configured for internal AGC. Vout is the output voltage swing at IF2 given in Vpp differential or rms.

Figure 4. IMD Level vs Input Power and AGC Output Setting (IF2 BPF Loss of 15 dB Included in Plot)

Figure 5. IMD Level vs Temperature at Output AGC Setting of 1.2-Vpp Differential (IF2 Filter Loss of 15 dB Included)

External Analog Control

Receive signal gain control can also be accomplished through direct interaction with the modem. For example, the modem can look at several metrics on the incoming signal including voltage swing, SNR, and AGC error, then feedback an analog (0 V to 3 V) gain control signal to the Texas Instruments ASIC. Note that for applications requiring large channel bandwidths (e.g., 6 MHz) the maximum usable VAGCI should be limited to approximately 2 V to 2.5 V, otherwise the resulting gain produces excessive amounts of noise at the output.

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Figure 6. TRF1112 / TRF1212 Gain vs AGCI Voltage (IF2 BPF Loss of 15 dB Included)

Figure 7 shows the input third-order intercept point (IIP3) vs V_{AGCI} for open loop AGC operation. As expected, the IIP3 decreases with increasing gain (increasing $\mathsf{V}_{\mathsf{AGCl}}$). The input P-1dB behaves in a similar way.

[Figure](#page-11-0) 8 shows that the output P-1dB (OP-1dB) and output (OIP3) of the TRF1112 / TRF1212 is approximately constant vs the V_{AGCI} voltage.

Figure 7. IIP3 vs AGCI Voltage and Temperature (IF2 BPF Loss of 15 dB Included)

Figure 8. OP-1dB and OIP3 vs AGCI Voltage and Temperature (IF2 BPF Loss of 15 dB Included)

INTEGRATED SYNTHESIZERS

PLL Programming

A UHF and S-band PLL are integrated in the TRF1112 / TRF1212. These two PLLs can be programmed via ^a 3-wire serial bus (CLK, DATA, and EN) from the baseband processor. The timing specs are given in the AC Timing table and detailed in Figure 9. [Figure](#page-12-0) 10details the addresses and register values required to fully program the synthesizers.

NOTE: If left unconnected, the DATA, CLK and EN pins rest on logic High.

Figure 9. Serial Interface Timing Diagram

Data is written to the PLLs according to the following format:

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The first eight bits are the appropriate address for the instruction set and the remaining 16 bits are the instructions. The data is 24 bits long (3 bytes). Byte 1 is the address with A[7] being the MSB and A[0] being the LSB. Byte 2 and 3 program the IC with synthesizer information and PS (polarity select bit) information. D[15] is the MSB and D[8] the LSB. The PS bit selects which edge of the reference is used for frequency comparison. Improved spurious and phase noise is achieved by selected the edge with the fastest rise or fall time. If $PS = 1$, the rising edge is used as the reference. If $PS = 0$, the falling edge is used.

The filter select (FS) bit selects which receive filter path is enabled. If FS = 1, the A filter path is selected, if FS = 0 the B filter path is selected. This feature allows the user to control the receive signal bandwidth.

Each of the three lines in Figure 10 needs to be sent to the TRF1112 /TRF1212 to fully program the synthesizers, the FS bit, and the PS bit. Once the synthesizers and the FS/PS bits are fully programmed, the clock signal should be turned off to eliminate any clock-associated spurious signals

The UHF oscillator (LO2) frequency of oscillation is set by the following equation:

$$
Fout = REFIN \times \left[8 \times (N+3) - S - \frac{F}{18}\right]/8
$$
\n(1)

The S-band oscillator (LO1) frequency of oscillation is set by the following equation:

$$
Fout = REFIN \times \left[8 \times (N+3) - S - \frac{F}{18}\right]
$$
 (2)

where F has a range of 0 to 17. Both N and S have ranges that are limited more by the LO range than by their digital count.

Both synthesizers use ^a fractional architecture, which allows ^a high comparison frequency relative to the step size. The S-band PLL operates at ^a reference frequency of 18 MHz with ^a minimum phase accumulator frequency of 1 MHz. The UHF PLL operates at ^a 9-MHz reference with ^a minimum phase accumulator frequency of 0.5 MHz. The S-band PLL has ^a step size of 1 MHz and the UHF PLL has ^a step size of 125 kHz, when using an 18-MHz reference frequency. Different reference frequencies yield different step sizes, many of which are non-integer. If ^a different reference frequency is chosen, the step size is linearly related to the step size for 18 MHz.

Step size = step size_{18MHz} x [REF FREQ/18 MHz]

In addition to normal reference spurious signals, fractional synthesizers have fractional spurs. The fractional spurs occur at an offset from the LO signal that is dependent on the difference between the LO frequency and integer multiples of the reference frequency. The spur locations can be found by the following process: divide the LO frequency by the reference frequency, take the remainder (fraction to the right of the whole number) and multiply by the reference frequency. This frequency is the difference between the actual LO frequency and an integer multiple of reference frequency. Fractional spurs will occur at this frequency and the reference frequency minus this frequency.

An example will best explain the process: if LO1 is set to 2206 MHz and an 18-MHz reference frequency is used, then 2206/18 is 122.55556. The difference between the LO1 and 122×18 MHz is:

 0.55556×18 MHz = 10 MHz

The fractional spurs will occur at this frequency offset (10 MHz) from LO1 and:

18 MHz–10 MHz or 8 MHz from LO1.

The fractional spurious level varies with the offset from the LO since these spurious signals are attenuated by the loop filter response. The larger the offset from the LO, the lower the spur level. In general, spurs at offsets greater than 3 or 4 MHz are below –75 dBc and are not ^a concern. The worst fractional spurs levels occur when they are located at 1 MHz offset from the LO1 frequency. (Note: the fractional spur is offset from the LO1 frequency by 1 MHz when the difference between the LO1 and an integer multiple of the reference frequency is 1 or 17 MHz.)

Although both synthesizers have fractional spurs, for most applications the spurious signals from the UHF (LO2) synthesizer can be ignored because these spurs are attenuated by frequency dividers that are placed after the LO2 generation. In some frequency plans it is possible to offset LO1 and LO2, in ^a complementary manner, to avoid worst-case fractional spurs (i.e., 1-MHz offsets) on LO1 synthesizer.

VCO Tuning Characteristics

The TRF1121 / TRF1221 internal VCOs have the following frequency vs tune voltage characteristics.

Figure 11. TRF1112 LO1 Frequency vs LO1TUN Voltage

Figure 14. TRF1212 LO2 Frequency vs LO2TUN Voltage

Phase Noise

The TRF1112 / TRF1212 achieve superior phase noise performance with on-chip resonators and varactors. They are designed to meet the phase noise requirements of both single carrier and multi-carrier systems. Due to chip architecture, the phase noise and spurious performance of the LO2 (UHF) PLL is about 15 dB better than the LO1 (S-band) PLL. The typical phase noise of the TRF1112 and TRF1212 S-Band PLL (LO1) with the PLL locked is shown in [Figure](#page-16-0) 15 and [Figure](#page-16-0) 16, respectively. The phase noise of the TRF1212 S-Band PLL at the min and max range are shown in [Figure](#page-18-0) 17 and Figure 18 respectively. These plots were taken at room temperature and typical voltage conditions.

Figure 15. Phase Noise of TRF1112 Synthesizer #1 – Typical Performance is 0.4 RMS (100 Hz to 1 MHz)

Figure 16. Phase Noise of the TRF1212 Synthesizer #1 – Typical Performance is 0.6 RMS (100 Hz to 1 MHz)

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Figure 17. TRF1212 S-Band Synthesizer Phase Noise - 2818 MHz

Figure 18. TRF1212 S-Band Synthesizer Phase Noise - 3418 MHz

For applications demanding tighter phase noise performance than that offered by Texas Instruments internal VCOs, ^a provision exists for connection of an external VCO. Texas Instruments integrated PLL locks the external VCO to the reference frequency and the chip provides an external tuning voltage that drives the VCO.

OUTPUT A/D INTERFACE

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The output of the baseband amplifier is designed to directly drive typical A/D inputs. The output IF2 buffer amplifiers are low impedance emitter followers as shown in [Figure](#page-19-0) 19.

Figure 19. Output Interface for TRF1112 / TRF1212

The peak current drive of the output transistors is 3 mA. Assuming ^a 1.2-Vpp differential (0.6 V single ended) voltage swing, the minimum impedance the TRF1112 / TRF1212 drives without clipping is 0.6 V/3 mA = 200 Ω, single-ended. In practice the impedance must be higher to prevent distortion products from degrading BER of the receiver. This impedance must include the A/D input capacitance and any parasitic board capacitance. At 44 MHz, the TRF1112 / TRF1212 drives a differential impedance of 1000 Ω (single ended impedance of 500 Ω) with up to a 10-pF capacitive load (293-Ω single-ended impedance) and maintain 38-dBc imtermodulation products with 64 QAM modulation. Proper attention to layout and reduction of parasitic capacitance at this interface is critical to avoid linearity degradation. At higher IF frequencies parasitic capacitance is even more critical.

If parasitic capacitance is loading the output and degrading intermodulation performance there are two approaches to solve the problem. First ^a shunt inductor can be added to resonate the capacitance. The inductor value would be determined by: L = $1/\omega^2$ Cp, where Cp is the parasitic capacitance and ω is 2π times the baseband receive IF frequency. Frequently this inductor can be part of the bias network for the ADC.

Second, the peak output current drive can be increased by adding ^a shunt resistor across the output of each baseband output. This resistor will essentially increase the quiescent current through the output transistor thus allowing ^a higher peak output current. The maximum **increase** in quiescent current is 3 mA resulting in ^a maximum allowable peak current of 6 mA. If load resistors are added, their resistance must be included to calculate total load impedance for the TRF1112 / TRF1212.

APPLICATION INFORMATION

A typical application schematic is shown in Figure 20 and ^a mechanical drawing of the package outline (LPCC Quad 7 mm \times 7 mm, 48-pin) is shown in [Figure](#page-21-0) 21.

Figure 20. Recommended TRF1112/TRF1212 Application Schematic

APPLICATION INFORMATION (continued)

Figure 21. Package Drawing

The recommended PCB Layout mask is shown in [Figure](#page-22-0) 22, along with recommendations on the board material (see Table 2) and construction (see [Figure](#page-23-0) 23).

SOLDER MASK: NO SOLDERMASK UNDER CHIP, ON LEAD PADS OR ON GROUND CONNECTIONS.

16 VIA HOLES, EACH 0.38 mm.

DIMENSIONS in mm

Figure 22. Recommended Pad Layout

Figure 23. PCB Via Cross Section

PACKAGING INFORMATION

(1) The marketing status values are defined as follows:

ACTIVE: Product device recommended for new designs.

LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

PREVIEW: Device has been announced but is not in production. Samples may or may not be available.

OBSOLETE: TI has discontinued the production of the device.

(2) Eco Plan - The planned eco-friendly classification: Pb-Free (RoHS), Pb-Free (RoHS Exempt), or Green (RoHS & no Sb/Br) - please check<http://www.ti.com/productcontent> for the latest availability information and additional product content details.

TBD: The Pb-Free/Green conversion plan has not been defined.

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(3) MSL, Peak Temp. -- The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

(4) Only one of markings shown within the brackets will appear on the physical device.

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REEL DIMENSIONS

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TAPE DIMENSIONS

TAPE AND REEL INFORMATION

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PACKAGE MATERIALS INFORMATION

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*All dimensions are nominal

MECHANICAL DATA

NOTES: A. All linear dimensions are in millimeters. Dimensioning and tolerancing per ASME Y14.5M-1994.

- B. This drawing is subject to change without notice.
- C. Quad Flatpack, No-leads (QFN) package configuration.

D. The package thermal pad must be soldered to the board for thermal and mechanical performance.

E. See the additional figure in the Product Data Sheet for details regarding the exposed thermal pad features and dimensions.

F. Falls within JEDEC MO-220.

RGZ (S-PVQFN-N48) PLASTIC QUAD FLATPACK NO-LEAD

THERMAL INFORMATION

This package incorporates an exposed thermal pad that is designed to be attached directly to an external heatsink. The thermal pad must be soldered directly to the printed circuit board (PCB). After soldering, the PCB can be used as a heatsink. In addition, through the use of thermal vias, the thermal pad can be attached directly to the appropriate copper plane shown in the electrical schematic for the device, or alternatively, can be attached to a special heatsink structure designed into the PCB. This design optimizes the heat transfer from the integrated circuit (IC).

For information on the Quad Flatpack No-Lead (QFN) package and its advantages, refer to Application Report, QFN/SON PCB Attachment, Texas Instruments Literature No. SLUA271. This document is available at www.ti.com.

The exposed thermal pad dimensions for this package are shown in the following illustration.

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